



# Efficiency of Target Location Scenarios in the Multi-Transmitter Multi-Receiver Passive Radar

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## Abstract

Multi-transmitter multi-receiver passive radar, which locates target in the surveillance area by the reflected signals of the available opportunistic transmitter from the target, is of interest in many applications. In this paper, we investigate different signal processing scenarios in multi-transmitter multi-receiver passive radar. These scenarios include decentralized processing of reference and surveillance signals, decentralized processing of surveillance signals, and centralized processing of surveillance signals that have different advantages, disadvantages, and requirements. A variety of possible measurements including TDOA, GROA, AOA and their combinations are presented under different scenarios. The Cramer Rao lower band (CRLB) is presented for different signal processing scenarios for the error of the target localization. The efficiency of the target localization for different signal processing scenarios and types of measurements has been investigated by the CRLB. As shown in the simulation results, the combined use of the measurements is always better than their single use. Also centralized and decentralized processing of surveillance signals, by arranging the receiver sensors in the far distances, can have better efficiency than close distance arrangements.

*Keywords:* Passive Radar, Multi-Transmitter Multi-Receiver Radar, Target Localization, Centralized Signal Processing, Decentralized Signal Processing.

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## 1. Introduction

Passive radar locates the target by receiving reflected signals from the target in the several receiver sensors. These signals are radiated by the transmitters existing in the environment called

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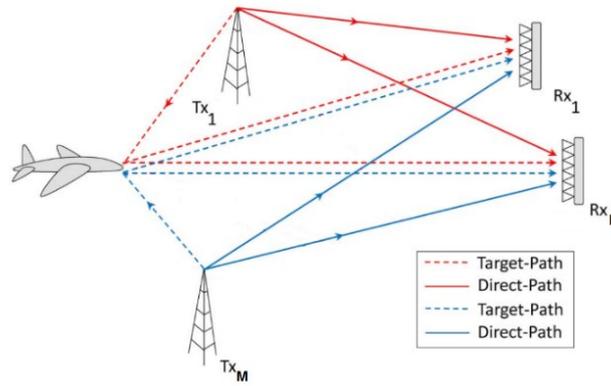


Figure 1: Geographic scheme of transmitters, receiver sensors, and target.

opportunistic transmitters. These radars for many years because of the features such as their latency in the magnetic spectrum, the low cost as compared to active radars, as well as no need of frequency allocation, have attracted much attention in various industries [1], [2], [3], [4], [5], [6], [7], [8], [9], [10]. latency in the frequency spectrum is due to the lack of signal radiation, cheapness as well as lack of need for frequency allocation due to not need on the transmitter. Various opportunistic transmitters, such as terrestrial broadcast transmitters including Radio FM, Digital Radio (DAB), Digital TV like DVB-T and DVB-T2 [11] have been investigated for use in the passive radar. On the other hand, various cellular telecommunication networks such as GSM [12], 3G and 4G [13] as well as Wi-Fi signals [14] and even satellite transmitters [15] such as GNSS [16] have also been investigated for this application [17], [18].

Target localization has been investigated under different scenarios such as active radars [19], [20]. Signal processing of passive radar is usually accomplished as multi-static active radars. Multi-static radar is created by the development of bistatic radars. In bistatic signal processing, it is necessary to receive the direct signal of the transmitter and the target reflection simultaneously. Target localization is done by extending or generalizing the bistatic radar to the multi-static radar [21], [22], [23]. Some processing scenarios and detection are reviewed by Hak [24], [25].

Localization of illuminator is studied in the context of passive source localization (PSL) [26], [27]. The effect of geographical topology has been investigated on PSL [28] that is similar to the centralized processing of reflected signals on the passive radar.

In this paper, we investigate different measurement scenarios for passive radars and their impact on localization efficiency. These measurements can be TDOA, GROA, and AOA measurements or a combination of them. Considering the arrangement of the receiver sensors, the possibility of receiving the transmitter signal has been investigated under different scenarios. Different signal processing scenarios including decentralized processing of transmitter signals and reflections in receiver sensors, the decentralized processing of reflected signals in the receiver sensors, and centralized processing of the reflected signals in the central sensor are investigated. In addition to signal processing scenario and receiver sensors arrangement, the network type of opportunistic transmitters also affects the localization efficiency. Localization scenarios have also been investigated for MFN and SFN networks. Investigations have been carried out for localization efficiency by presenting the CRLB under different scenarios using the presented procedure in [28], [29]. The advantages and disadvantages of different scenarios are presented by the simulation results. The structure of this paper is as described in Section 2 of the Signal Model and Measurements. Different scenarios and their requirements are presented in section 3. Simulations and conclusions are presented in sections 4 and 5 respectively.

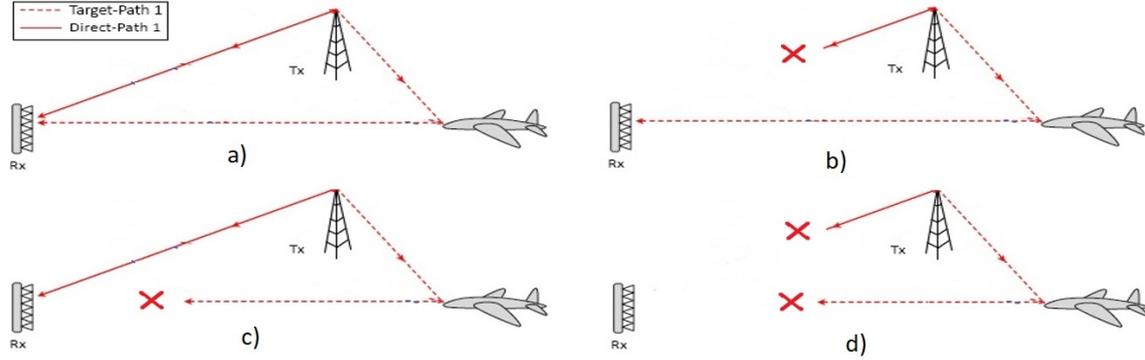


Figure 2: Different scenarios of receiving reference signals and surveillance signals

## 2. System model

Passive radar uses opportunistic transmitters in the environment. The target reflected signal is received by the receiver sensors in the passive radar. The geographical scheme of the problem is illustrated in Fig. 1. As shown, the  $M$  opportunistic transmitters radiate signals in the environment. The reflected signals from the target are received by the  $N$  receiver sensors. The receiver sensors use two separate channels to receive the direct path signal of the transmitter and the target reflection. Direct path signals are received from the reference channel while the reflected signals from the surveillance channel. The reference channel uses the directional antenna to receive the direct signal of the transmitter whereas the surveillance channel uses an array of omnidirectional antennas to receive the reflections.

### 2.1. Bistatic Scenario

The multi-transmitter multi-receiver passive radar system model, such as the MIMO radar is considered with the separated antennas. In the passive radar scenario, the transmitter is not under control of radar designers, and the transmitters are usually placed at large distances with each other to cover the under service area. However, the receiver sensors can be located at close distances. Passive radar processing is based on bistatic radar processing. Each pair of the bistatic signal consists of two signals of the transmitter and the target reflection. In the passive radar, several scenarios may occur for each pair of bistatic signals as shown in Fig. 2. These scenarios are developed by assuming the receiving or not receiving each of the direct path signals and/or the reflection and include:

- a) Receive both direct signal and reflection in the receiver.
- b) Receive only the reflection signal.
- c) Receive only direct signal.
- d) Receive none of the signals.

$$s_{STx_i, Ta, Rx_j}(t) = \frac{1}{g_{Tx_i, Ta, Rx_j}} s_{Tx_i}(t - \tau_{Tx_i, Ta, Rx_j}) a(\theta_{Ta, Rx_j}, \phi_{Ta, Rx_j}) \quad (2.1)$$

$$s_{r_{Tx_i, Rx_j}}(t) = \frac{1}{g_{Tx_i, Rx_j}} s_{Tx_i}(t - \tau_{Tx_i, Rx_j}) a(\theta_{Tx_i, Rx_j}, \phi_{Tx_i, Rx_j}) \quad (2.2)$$

$$\tau_{Tx_i, Rx_j} = \frac{r_{Tx_i, Rx_j}}{c} \quad (2.3)$$

$$\tau_{Tx_i, Ta, Rx_j} = \frac{r_{Tx_i, Ta} + r_{Ta, Rx_j}}{c} \quad (2.4)$$

$$g_{Tx_i, Rx_j} = \frac{(r_{Tx_i, Rx_j})^\gamma}{A_{Tx_i, Rx_j} A_{Rx_j, Tx_i}} F \quad (2.5)$$

$$g_{Tx_i, Ta, Rx_j} = \frac{(r_{Tx_i, Ta} r_{Ta, Rx_j})^\gamma}{A_{Tx_i, Ta} \sqrt{\sigma_{Tx_i, Ta, Rx_j}} A_{Rx_j, Ta}} F \quad (2.6)$$

$$\theta_{Tx_i, Rx_j} = \arctan\left(\frac{y_{Ta} - y_{Rx_j}}{x_{Ta} - x_{Rx_j}}\right) \quad (2.7)$$

$$\phi_{Ta, Rx_j} = \arcsin\left(\frac{z_{Ta} - z_{Rx_j}}{r_{Ta, Rx_j}}\right) \quad (2.8)$$

The above modes are different for each pair of bistatic signals per receiver, depending on the processing scenario, the transmitters and receiver sensors arrangement, the target location and the area geography.

## 2.2. Signal model

Locations of transmitters are shown  $\underline{p}_{Tx_i} = [x_{Tx_i} \ y_{Tx_i} \ z_{Tx_i}]^T$  by and Locations of receiver sensors are shown by  $\underline{p}_{Rx_j} = [x_{Rx_j} \ y_{Rx_j} \ z_{Rx_j}]^T$ . Where,  $i$  and  $j$  are the transmitter index and the receiver index, respectively. The target is located at  $\underline{p}_{Ta} = [x_{Ta} \ y_{Ta} \ z_{Ta}]^T$ . The reflected signal of transmitter  $i$  received by sensor  $j$  from the target which is presented in equation (2.1) and the received direct signal of transmitter  $i$  is presented in equation (2.2).

In these equations,  $sr_{Tx_i, Rx_j}(t)$  is the received reference signal,  $ss_{Tx_i, Ta, Rx_j}(t)$  is reflected signal received from the target,  $st_{Tx_i}(t)$  is transmitted signal of transmitter  $i$ ,  $\tau$  shows the path delay,  $g$  depicts the path attenuation,  $\theta_{Ta, Rx_j}$  and  $\phi_{Ta, Rx_j}$  are the direction of arrival of the received signal in receiver  $j$ .  $a(\theta_{Ta, Rx_j}, \phi_{Ta, Rx_j})$  is the signal angular function of the reflection received from the target at the receiver location. The values of these parameters depending on the characteristics of the target, transmitter, and receiver sensor are given in equations (2.3) to (2.8).

In equation (5) and (6), the  $A_{x,y}$  is gain of  $x$ 's antenna in the  $y$  direction,  $\sigma_{Tx_i, Ta, Rx_j}$  is the target RCS value in bistatic angle of transmitter  $i$ , target, and receiver  $j$ ,  $r_{x,y} = \|\underline{p}_x - \underline{p}_y\|$  is distance between  $\underline{p}_x$  and  $\underline{p}_y$ ,  $c$  is the signal propagation speed,  $\gamma$  is the path loss component which usually considered equal to 1, and  $F$  denote other fixed parameters.  $\|\underline{x}\|$  shows the norm of vector  $\underline{x}$ . It should be noted that by point target assumption that is true for the far-field target, the value of  $\sigma_{Tx_i, Ta, Rx_j}$  is equal for all couples of receivers and transmitters and is denoted by  $\sigma$ . Assuming the transmitter and receiver locations are known, the direct signal will be independent of the angular function and  $a(\theta_{Ta, Rx_j}, \phi_{Ta, Rx_j})$  can be considered equal to 1 in the equation. In fact, the receiver sensor by directing the antenna to the transmitter receives the direct signals of the transmitter with maximum gain. Also assuming an omnidirectional antenna for the transmitter in the signal transmission, then the value of  $A_{Tx_i, Ta}$  is independent of the target location and the value of  $A_{Tx_i, Rx_j}$  is independent of the receiver location. Therefore, both parameters will be constant and equal to  $A_{Tx_i}$ . Furthermore, assuming an omnidirectional antenna for the receivers sensors, the parameter  $A_{Ta, Rx_j}$  independent of the target location will be equal to  $A_{Rx_j}$ .

## 2.3. Measurements model

The signals are processed after detection in the receiver sensors. The bistatic signal detection includes receiving or not receiving the direct path signal and the reflection signal. After detection, if there is a direct transmitter signal in the receiver sensor, its effect must be removed from the surveillance channel. Then the time and/or power and/or direction and/or the doppler of received

reflected signal from the target are calculated. The target reflection signal is required for location processing. Therefore, two scenarios of receiving the reflection signal in the presence and absence of the direct transmitter signal are used for subsequent passive radar processing, including the target localization and tracking. Three types of reflection signals measurement can be performed that include TDOA, GROA, and AOA. The measurement vector is equal to:

$$\underline{k} = [\underline{\tau}^T \quad \underline{g}^T \quad \underline{\theta}^T \quad \underline{\phi}^T]^T \quad (2.9)$$

In the above equations of  $\underline{k}$ ,  $\underline{\tau}$ ,  $\underline{g}$ ,  $\underline{\theta}$ , and  $\underline{\phi}$  vectors are in the order of the vectors of all measurements, the TDOA, GROA, and DOA measurements respectively, azimuth angle and elevation angle of DOA measurements. The measurement of these vectors is associated with the noise that we model as additive noise. For the simplicity of calculations, we assume the measurement noises as additive Gaussian noise. Therefore, the measurement vector is equal to:

$$\underline{k} = \hat{\underline{k}} + n_{\hat{\underline{k}}} \quad (2.10)$$

$$n_{\hat{\underline{k}}} \sim N(0, Q); \text{diag}(Q) = [\underline{\sigma}_{\tau}^{2T} \quad \underline{\sigma}_g^{2T} \quad \underline{\sigma}_{\theta}^{2T} \quad \underline{\sigma}_{\phi}^{2T}]^T \quad (2.11)$$

In the above equation,  $\hat{\underline{k}}$  the vector represents the non-noise values of the measurements.  $\underline{\sigma}_{\tau}^2$ ,  $\underline{\sigma}_g^2$ ,  $\underline{\sigma}_{\theta}^2$ , and  $\underline{\sigma}_{\phi}^2$  are the noise variance vectors of TDOA measurements, the noise of GROA measurement, noise of DOA measurement of azimuth angle and the noise of elevation angle measurements. Other scenarios of measurements are obtained by simplifying and reducing these vectors. These modes include alone TDOA, alone AOA, TDOA and AOA, TDOA and GROA, AOA and GROA.

### 3. Performance of target localization for different measurement scenarios

In the passive radar, the measurements accomplished by receiver sensors are dispatched to the central sensor for target locating and tracking. The central sensor engages in locating and tracking the target by per knowledge of locations of the receiver sensors and opportunistic transmitters and measurements taken at the receiver sensors. As mentioned, the available measurements include TDOA, GROA, and AOA. The measurement vector used for locating is shown in equation (2.10). All or some of these measurements can be used according to the scenario.

Measurements calculation on the passive radar by processing the received signals can be done centralized on the central sensor or decentralized on the receiver sensors. In the centralized processing scenario, the signals are dispatched to the central sensor and part of signal processing is carried out there. In the decentralized processing scenario, signal processing is performed only on the receiver sensors and the measurements are sent to the central sensor. In the locating process, data association is a fundamental step. The data association involves specifying the opportunistic transmitter of the radiation's received reflection on one hand and specifying the measurements done related to one target in different receiver sensors on the other hand. This measurement allocation also depends on the type of opportunistic transmitters network topology. That is, after calculating the measurements, it must be determined which measurements belong to a specific target and which transmitter was the source of radiations. In some methods, this is done by considering all possible modes by MHT tracking algorithms [30].

$$\underline{\tau} = \left[ \mathcal{T}_{Tx_1, Ta, Rx_1; Tx_1, Rx_1} \quad \cdots \quad \mathcal{T}_{Tx_1, Ta, Rx_N; Tx_1, Rx_N} \quad \cdots \quad \mathcal{T}_{Tx_M, Ta, Rx_1; Tx_M, Rx_1} \quad \cdots \quad \mathcal{T}_{Tx_M, Ta, Rx_N; Tx_M, Rx_N} \right]^T \quad (3.1)$$

$$\tau_{Tx_i, Ta, Rx_j; Tx_i, Rx_j} = \tau_{Tx_i, Ta, Rx_j} - \tau_{Tx_i, Rx_j} = \frac{r_{Tx_i, Ta, Rx_j} - r_{Tx_i, Rx_j}}{c} = \frac{r_{Tx_i, Ta} + r_{Ta, Rx_j} - r_{Tx_i, Rx_j}}{c} \quad (3.2)$$

$$\underline{\tau} = \left[ \tau_{Ta, Rx_2; Ta, Rx_1 | Tx_1} \quad \cdots \quad \tau_{Ta, Rx_N; Ta, Rx_1 | Tx_1} \quad \cdots \quad \tau_{Ta, Rx_N; Ta, Rx_{N-1} | Tx_1} \quad \cdots \quad \tau_{Ta, Rx_N; Ta, Rx_{N-1} | Tx_M} \right]^T \quad (3.3)$$

$$\tau_{Ta, Rx_j; Tx_i, Rx_1 | Tx_i} = \tau_{Ta, Rx_j} - \tau_{Ta, Rx_1} = \frac{r_{Ta, Rx_j} - r_{Ta, Rx_1}}{c} \quad (3.4)$$

$$\underline{\tau} = \left[ \tau_{Ta, Rx_2; Ta, Rx_1 | Tx_1} \quad \cdots \quad \tau_{Ta, Rx_N; Ta, Rx_1 | Tx_1} \quad \cdots \quad \tau_{Ta, Rx_2; Ta, Rx_1 | Tx_M} \quad \cdots \quad \tau_{Ta, Rx_N; Ta, Rx_1 | Tx_M} \right]^T \quad (3.5)$$

$$\tau_{Ta, Rx_j; Tx_i, Rx_1 | Tx_i} = \tau_{Ta, Rx_j} - \tau_{Ta, Rx_1} = \frac{r_{Ta, Rx_j} - r_{Ta, Rx_1}}{c} \quad (3.6)$$

$$\underline{g} = \left[ g_{Ta, Rx_2; Ta, Rx_1 | Tx_1} \quad \cdots \quad g_{Ta, Rx_N; Ta, Rx_1 | Tx_1} \quad \cdots \quad g_{Ta, Rx_2; Ta, Rx_1 | Tx_M} \quad \cdots \quad g_{Ta, Rx_N; Ta, Rx_1 | Tx_M} \right]^T \quad (3.7)$$

$$g_{Ta, Rx_j; Tx_i, Rx_1 | Tx_i} = \frac{g_{Ta, Rx_j | Tx_i}}{g_{Ta, Rx_1 | Tx_i}} = \frac{\sqrt{\sigma_{Tx_i, Ta, Rx_1}} A_{Rx_1, Ta} r_{Ta - Rx_j}}{\sqrt{\sigma_{Tx_i, Ta, Rx_j}} A_{Rx_j, Ta} r_{Ta - Rx_1}} \quad (3.8)$$

$$\underline{\theta} = \left[ \theta_{Ta, Rx_1 | Tx_1} \quad \cdots \quad \theta_{Ta, Rx_N | Tx_1} \quad \cdots \quad \theta_{Ta, Rx_1 | Tx_M} \quad \cdots \quad \theta_{Ta, Rx_N | Tx_M} \right]^T \quad (3.9)$$

$$\theta_{Ta, Rx_j | Tx_i} = \text{atan}\left(\frac{(\underline{p}_{Ta} - \underline{p}_{Rx_j}) \underline{y}_T}{(\underline{p}_{Ta} - \underline{p}_{Rx_j}) \underline{x}^T}\right); \underline{x} = [1 \ 0 \ 0]^T; \underline{y} = [0 \ 1 \ 0]^T \quad (3.10)$$

$$\underline{\phi} = \left[ \phi_{Ta, Rx_1 | Tx_1} \quad \cdots \quad \phi_{Ta, Rx_N | Tx_1} \quad \cdots \quad \phi_{Ta, Rx_1 | Tx_M} \quad \cdots \quad \phi_{Ta, Rx_N | Tx_M} \right]^T \quad (3.11)$$

$$\phi_{Ta, Rx_j | Tx_i} = \text{asin}\left(\frac{(\underline{p}_{Ta} - \underline{p}_{Rx_j}) \underline{z}_T}{r_{Ta, Rx_j}}\right); \underline{z} = [0 \ 0 \ 1]^T \quad (3.12)$$

In addition to the method of signal processing, the network topology of used opportunistic transmitters affect computing the measurement vectors. The network of opportunistic transmitters is MFN or SFN. In MFN networks, such as a transmitters network with different frequencies, the signals of opportunistic transmitters are separable in the receiver sensors. Thus, using the MFN transmitters, each receiver sensor can receive a target reflection against each opportunistic transmitter. In this case, the data association only involves specifying the measurements related to a target. In SFN networks, the opportunistic transmitters signals are not separable. Like the transmitters use the same frequency. Therefore, the receiver sensors receive only a reflection from the target resulting from the strongest transmitter signal. data association in addition to specifying measurements related to a target also involves determining the transmitter of the received reflection signal. In the following, the measurement vectors are presented for these scenarios.

### 3.1. Measurement vectors

This section presents measurement vectors under different processing scenarios. Considering two centralized and decentralized processing scenarios and two signal reception scenarios, reflections are provided in the presence or absence of a direct transmitter signal. We have three different scenarios for TDOA measurements: Decentralized processing of reference-surveillance channels, centralized processing of surveillance channels and decentralized processing of surveillance channels. In all cases, GROA and DOA measurements are calculated by the decentralized processing of surveillance channels. The total number of measurements for different scenarios is presented in Table 1.

#### 3.1.1. TDOA measurements vector for decentralized processing of reference-surveillance channels

Both signals of the transmitter direct path and the target reflection are received in this scenario. The TDOA measurements are computed by decentralized processing of direct path signal received from the reference channel and the reflection signal received from the surveillance channel in the receiver sensors. In an MFN network, the number of  $M$  TDOA measurements can be calculated between the reference and surveillance channels in each receiver sensor presented by the measurement vectors in equation (3.1). TDOAs can be obtained from cross ambiguity function of surveillance-reference channels. In the MFN network, there are  $M \times (N-1)$  measurements. In the SFN network, we have  $N$  TDOA measurements that the  $Tx_i$  change to  $Tx_s$  in equation (3.1). Where,  $s$  indicates the index of the strongest transmitter in that receiver. In these equations  $\tau_{Tx_i, Ta, Rx_j; Tx_i, Rx_j}$  is presented in equation (3.2).

#### 3.1.2. TDOA measurements vector in centralized processing of surveillance channels

In this scenario, independent of whether or not to receive the direct path transmitter signal, all received reflections sampled at the receiving sensor must be transmitted to the central sensor. The TDOAs in the central sensor are calculated by processing the reflected signals received from the surveillance channels in the different receiver sensors relative to all other receiver sensors. TDOAs can be obtained from the cross ambiguity function of surveillance channels. In an MFN network, we have  $(N-1)/2$  measurements for TDOA per each transmitter and compared to the surveillance channels of both receiver couples; the measurement vectors are presented in equation (3.3). In the SFN network, we have  $(N-1)/2$  number of TDOA measurements. In equation (3.3), the  $Tx_i$  changes to  $Tx_s$  only. In these equations,  $\tau_{Ta, Rx_j, Ta, Rx_k | Tx_s}$  is shown in equation (3.4).

#### 3.1.3. TDOA measurements vector in decentralized processing of surveillance channels

In this scenario, independent of whether receiving or not receiving the direct path signal of the transmitters, received reflections are processed in the receiving sensors themselves. All receiver sensors must be synchronous with each other in clock and time reference. Signal processing is performed on each receiver sensor and calculated time of arrival (TOA) of reflection is transmitted to the central sensor. In the central sensor, the TDOA measurements are obtained from the difference of estimated TOA measurements of relations in the receiver sensors. To obtain TDOA, one has to use a specific pattern in the transmitter signal or a specific criterion in the receiver. In an MFN network, we have  $(N-1)$  number TDOA and GROA measurements per each transmitter. The measurement vectors are presented in equation (3.5). in the SFN network, we have  $(N-1)$  number TDOA measurements that the  $Tx_i$  change to  $Tx_s$  in equation (3.5). In these equations,  $\tau_{Ta, Rx_j, Ta, Rx_1 | Tx_s}$  is presented in equation (3.6).

#### 3.1.4. GROA measurement vectors

Each receiver sensor can estimate the power of the received reflection by the processing of received signals. The GROA measurements are obtained by dividing the inverse square of the estimated power

in the receiver sensors by the estimated power in reference receiver sensor. In an MFN network, we have the  $N - 1$  number of measurements per transmitter. The measurement vectors are presented in equation (3.7). In the SFN network, we have 1 measurement in each receiver sensor against each strongest transmitter that the  $Tx_i$  change to  $Tx_s$  in this equation. Where,  $s$  indicates the index of the strongest transmitter in that receiver. In this equation,  $g_{Ta, Rx_j; Tx_i, Rx_l | Tx_i}$  are presented in equation (3.8).

### 3.1.5. DOA measurement vectors

Each receiver sensor can estimate the direction of the received reflection by the processing of received signals from the antenna array. In an MFN network, we have the  $N$  number of measurements per transmitter. The measurement vectors are presented in equations (3.9) and (3.10). In the SFN network, we have 1 measurement in each receiver sensor against each strongest transmitter that the  $Tx_i$  change to  $Tx_s$  in these equations. Where,  $s$  indicates the index of the strongest transmitter in that receiver. In these equation,  $\theta_{Ta, Rx_j}$  and  $\phi_{Ta, Rx_j}$  are presented in equation (3.11) and (3.12), respectively.

### 3.1.6. Rao Cramer Lower Band (CRLB)

This section presents a lower band of location estimation errors in multi-transmitter multi-receiver passive radar by TDOA, GROA, and AOA measurements. Assuming the noises of measurements are additive and Gaussian, the CRLB is obtained by using the Fisher Matrix to fit the used measurements and independent of the signal type. CRLB Matrix for  $\underline{p}_{Ta}$  is equal to [31]

$$CRLB = FIM_{-1}(\underline{p}_{Ta}) \quad (3.13)$$

The FIM matrix represents the Fisher information matrix. Assuming the additive Gaussian noise assumption of measurement vector  $k$  FIM matrix is equal to

$$FIM(\underline{p}_{Ta}) = \left( \frac{\partial \underline{k}}{\partial \underline{p}_{Ta}^T} \right)^T Q^{-1} \left( \frac{\partial \underline{k}}{\partial \underline{p}_{Ta}^T} \right) \quad (3.14)$$

$\partial \underline{k} / \partial \underline{p}_{Ta}^T$  should be calculated for TDOA, GROA, and AOA measurements under centralized and decentralized processing scenarios. This value for TDOA measurements with decentralized processing scenarios of surveillance-reference channels, centralized processing of surveillance channels and decentralized processing of surveillance channels is presented in equations (3.15), (3.16), (3.17), and for GROA and AOA measurements by decentralized processing of surveillance, channel is presented in equations (3.18) and (3.19), respectively.

$$\frac{\partial_{Tx_i, Ta, Rx_j; Tx_i, Rx_j}}{\partial \underline{p}_{Ta}^T} = \frac{1}{c} \left( \frac{[\underline{p}_{Ta} - \underline{p}_{Tx_i}]^T}{r_{Tx_i, Ta}} + \frac{[\underline{p}_{Ta} - \underline{p}_{Rx_j}]^T}{r_{Rx_j, Ta}} \right) \quad (3.15)$$

$$\frac{\partial_{Ta, Rx_j; Ta, Rx_l}}{\partial \underline{p}_{Ta}^T} = \frac{1}{c} \left( \frac{[\underline{p}_{Ta} - \underline{p}_{Rx_j}]^T}{r_{Ta, Rx_j}} - \frac{[\underline{p}_{Ta} - \underline{p}_{Rx_l}]^T}{r_{Ta, Rx_l}} \right) \quad (3.16)$$

$$\frac{\partial g_{Ta, Rx_j; Ta, Rx_l}}{\partial \underline{p}_{Ta}^T} = \frac{A_{Rx_l, Ta}}{A_{Rx_j, Ta}} \sqrt{\frac{\sigma_{Tx_i, Ta, Rx_l}}{\sigma_{Tx_i, Ta, Rx_j}}} \frac{r_{Ta, Rx_j}}{r_{Ta, Rx_l}} \left( \frac{[\underline{p}_{Ta} - \underline{p}_{Rx_j}]^T}{r_{Ta, Rx_j}^2} - \frac{[\underline{p}_{Ta} - \underline{p}_{Rx_l}]^T}{r_{Ta, Rx_l}^2} \right) \quad (3.17)$$

$$\frac{\partial \theta_{Ta, Rx_j}}{\partial \underline{p}_{Ta}^T} = \frac{1}{l_{Ta, Rx_j}^2} \left( ([\underline{p}_{Ta} - \underline{p}_{Rx_j}]^T \underline{x}) \underline{y} - [\underline{p}_{Ta} - \underline{p}_{Rx_j}]^T \underline{y} \underline{x} \right) \quad (3.18)$$

$$\frac{\partial g_{T_a, R_{x_j}; T_a, R_{x_l}}}{\partial \underline{p}_{T_a}^T} = \frac{A_{R_{x_l}, T_a} \sigma_{T_{x_i}, T_a, R_{x_l}} r_{T_a, R_{x_j}}}{A_{R_{x_j}, T_a} \sigma_{T_{x_i}, T_a, R_{x_j}} r_{T_a, R_{x_l}}} \left( \frac{[\underline{p}_{T_a} - \underline{p}_{R_{x_j}}]^T}{r_{T_a, R_{x_j}}^2} - \frac{[\underline{p}_{T_a} - \underline{p}_{R_{x_l}}]^T}{r_{T_a, R_{x_l}}^2} \right) \quad (3.19)$$

The matrix  $Q$  in equation (3.14) represents the covariance. The elements of this matrix are provided for the TDOA, GROA, and AOA dependent on the transmitted signal specifications and SNR value. On the other hand, the SNR of the received signal for the reflected signals. As obvious, the SNR is dependent on the range. Hence, regardless of the transmitter signal specification, the efficiency of locating through dependence on the variance of the measurements is dependent also on the inverse of square of range.

#### 4. Simulation result

In this section, we present the simulation results of different processing scenarios. The Lower band of RMSE (Root Mean Square Error) of target location estimating will be provided with the square root of CRLB. The amount provided is of variable length and in meters. The simulations are presented in 3 different categories. The first section investigates the impact of the target location on the CRLB. In this case, the simulation results are shown with the colored contours, which indicate the RCRLB on the two-dimensional plane. These simulations provide an overview of the impact of the target location and the comparison of different scenarios. The second section investigates the impact of errors on different processing scenarios. In this case, the advantages and disadvantages of the scenarios will be observed for a variety of measurement errors. In the third cluster, the dependence of the accuracy of the measurement on the range is investigated. The locations of the transmitters are presented in Table (1). We consider the location of the receiver sensors under two categories of close distance and far distance sensors. Locations of receiver sensors in the close distance arrangement are presented in Table (2) and for the far distance arrangement is presented in Table (3).

##### 4.1. Impact of the target location

we Consider an area contains  $x$  and  $y$  equal to of AA and AA respectively in the Cartesian coordinates. The target altitude is considered equal to 9km in this area. We present the RCRLB value at different locations in this space. We also investigate several different arrangement scenarios. The sensors are assumed to use TDOA and azimuth angle of AOA measurements. The standard deviation of measurement errors for the time difference of arrival and direction of arrival are assumed equal to 100ns and 1deg respectively for different points of space. As shown in figures (3) to (6) for the different sensors arrangement of the receiver sensors. Centralized processing of surveillance channels performs better than decentralized processing of surveillance channels, but their performances are close together. processing of surveillance channels by far distance arrangement of receiver sensors has better performance than decentralized processing of reference-surveillance channels by close distance arrangement of receiver sensors. However, each of these processing scenarios has different requirements and limitations.

Table 1: Transmitters

index	x	y	z
1	0km	0km	100m
2	20km	20km	100m
3	-20km	20km	100m

Table 2: Receivers sensors in close arrangement

index	x	y	z
1	0	0	100m
2	10km	10km	200m
3	-10km	10km	200m
4	0	20km	100m

Table 3: Receivers sensors in the far arrangement

index	x	y	z
1	0	0	100m
2	50km	50km	200m
3	-50km	50km	200m
4	0	100km	100m

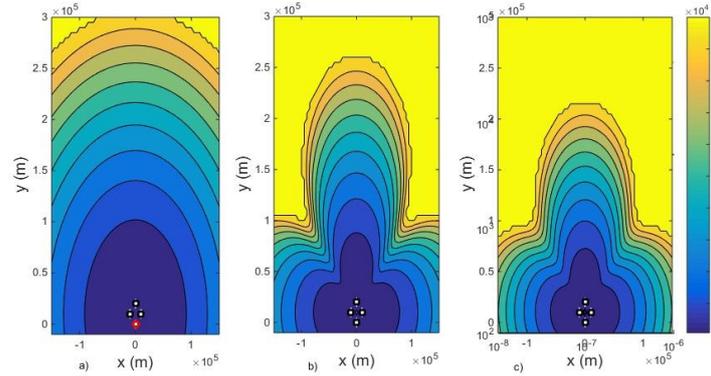


Figure 3: RCRLB on plane  $x$  and  $y$  for TDOA and AOA azimuth angle measurements with standard deviations of measurements errors equal to 100ns and 1deg respectively, by one transmitter and 4 receivers at close range for a) decentralized processing of reference-surveillance channels, b) centralized processing of surveillance channels, and c) decentralized processing of surveillance channels.

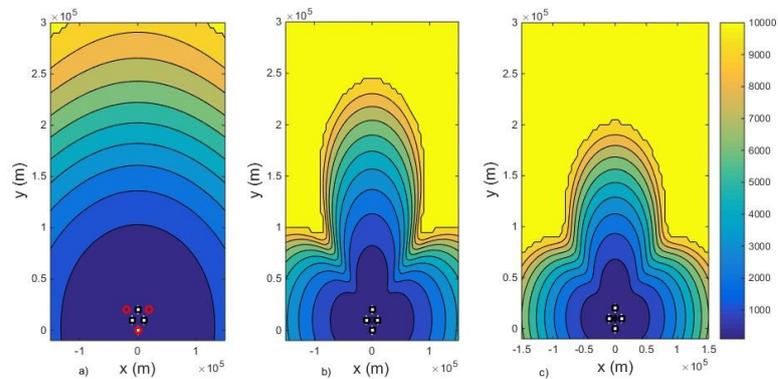


Figure 4: RCRLB on plane  $x$  and  $y$  for TDOA and AOA azimuth angle measurements with standard deviations of measurements errors equal to 100ns and 1deg respectively, by 3 transmitters and 4 receivers at close range for a) decentralized processing of reference-surveillance channels, b) centralized processing of surveillance channels, and c) decentralized processing of surveillance channels.

#### 4.1.1. A transmitter and close distance receiver sensors

In this scenario, the locations of receiver sensors are considered in accordance with Table (2) and only the first transmitter of the Table (1) is considered. The RCRLB value is shown for different locations in the area. Fig. 3 (a) shows the decentralized processing of the reference-surveillance channels. Figure b) shows the centralized processing of surveillance channels and figure c) shows the decentralized processing of surveillance channels. As shown, the RCRLB is limited to 20km. Decentralized processing of surveillance-reference channels has better efficiency than the other two methods. Furthermore, centralized processing of surveillance channels has better efficiency than the decentralized processing of them. however, this difference is low and performance is close together.

#### 4.1.2. Three transmitters and close distance receiver sensors

In this scenario, we consider the locations of the transmitters according to Table (1) and the receiver sensors according to Table (2). The transmitter network is considered as MFN and it is assumed that reflections caused by different transmitters' radiations can be separated from each other. The RCRLB value is shown for different locations of the area. Fig. 4 (a) shows the decentralized processing of the reference-surveillance channels, figure b) shows the centralized processing of surveil-

lance channels, and figure c) shows the decentralized processing of surveillance channels. As shown, the RCRLB is limited to 10km. The use of decentralized processing of the reference-surveillance channel is better than the other two methods. The centralized processing of surveillance channels has better efficiency than the decentralized processing of them.

#### 4.1.3. A transmitter and far distance receiver sensors

In this scenario, the locations of the receiver sensors are considered according to Table (3) and only the first transmitter of Table (1) is considered. The RCRLB value is shown for different locations of the area. Fig. 5 (a) shows centralized surveillance channels processing and figure b) shows decentralized processing of surveillance channels. The decentralized processing of reference-surveillance channels is not presented due to the impossibility of receiving the reference signal in this scenario. As shown, the RCRLB is limited to 10 km. The use of centralized processing of surveillance channels performs better than decentralized processing of surveillance channels, but their difference is low and the performances are close together. As it is obvious, the efficiency of centralized processing of surveillance channels by this far distance arrangement of receiver sensors is better than the decentralized processing of surveillance-reference channels by close distance arrangement of the receiver sensors.

#### 4.1.4. Three transmitters and far distance receiver sensors

In this scenario, we consider the locations of the transmitters according to Table (1) and the receiver sensors according to Table (3). The transmitter network is considered as MFN and it is assumed that reflections caused by different transmitters' radiations can be separated from each other in the receiver sensors. The RCRLB value is shown for different locations in the area. Fig. 6 a) shows the centralized processing of surveillance channels and figure b) shows the decentralized processing of surveillance channels. Decentralized processing of reference-surveillance channels is not provided like the previous scenario. As shown, the RCRLB is limited to 5km. The use of centralized processing of surveillance channels performs better than the decentralized processing of them, but their difference is low and the performances are close together. As it is obvious, the efficiency of centralized processing of surveillance channels by this far arrangement of receiver sensors is better than the decentralized processing of surveillance-reference channels by the close arrangement of receiver sensors.

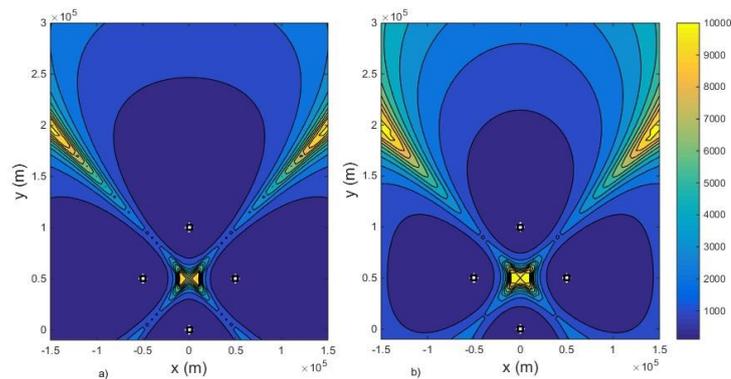


Figure 5: RCRLB on plane  $x$  and  $y$  for TDOA and AOA azimuth angle measurements with standard deviations of measurements errors equal to 100ns and 1deg respectively, by 1 transmitter and 4 receivers at a distance for a) centralized processing of surveillance channels and b) decentralized processing of surveillance channels.

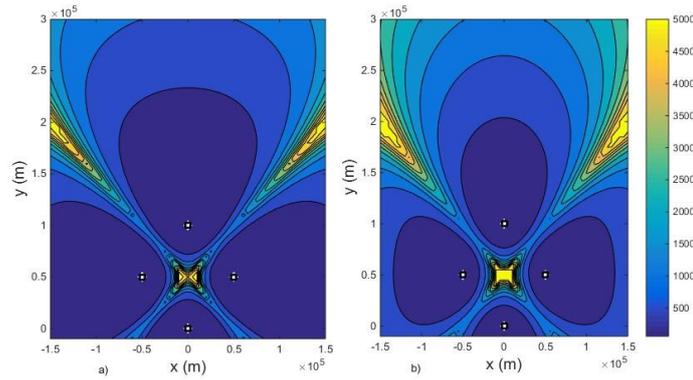


Figure 6: RCRLB on plane  $x$  and  $y$  for TDOA and AOA azimuth angle measurements with standard deviations of measurements errors equal to 100ns and 1deg respectively, by 3 transmitters and 4 receivers at a remote distance for a) centralized processing of surveillance channels and b) decentralized processing of surveillance channels.

#### 4.2. Effect of measurements errors

In this section, we present the impact of measurement errors on estimation efficiency by investigation of the lower band of error. The target is considered at  $\underline{p}_{Ta} = [40km \ 80km \ 9km]^T$ . We consider the transmitters of Table (1) and the arrangement of the receiver sensors as close distance in Table (2). Because of the far distance of the target to the transmitters and receiver sensors, we model it as point target and so it will be possible to use GROA measurements and its independence from the target RCS. Fig. 7 shows RCRLB vs standard division of TDOA error and Fig. 8 shows RCRLB vs the standard division of AOA error. The RCRLBs are shown for the scenarios of measurements include TDOA alone, AOA alone, TDOA and AOA combination and TDOA, GROA, and AOA combination in these figures. As illustrated, combined measurement mode has better efficiency than alone using of each measurement. As illustrated, CRLB of combined measurements is a function of measurement with a lower CRLB. where the CRLB of measurements is approximately equal, the Improvement caused by the combined use of measurements is more evident.

##### 4.2.1. TDOA measurement error

Fig. 7 shows the RCRLB value vs standard deviation of the TDOA error from 10ns to 1us. The standard deviation of the azimuth angle and elevation angle of AOA measurement errors is 1deg and 5deg respectively. The standard deviation of GROA is considered equal to -15dB. Figure a) shows the decentralized processing efficiency of the reference-surveillance channels. Figures b) and c show the centralized processing of surveillance channels and the decentralized processing of them, respectively. As shown, the combined use of TDOA, GROA, and AOA measurements has better efficiency than other cases.

##### 4.2.2. AOA measurement error

Figure 8 shows the RCRLB value vs standard deviation of the azimuth angle of AOA error from 0.1deg to 5deg. The standard deviation of the elevation angle of AOA measurement errors is assumed to be 5deg, TDOA measurement errors equal to 100ns, and GROA measurement errors equal to 15dB. Figure a) shows the decentralized processing efficiency of the reference-surveillance channels. Figures b) and c show the centralized processing of surveillance channels and decentralized processing of them, respectively. like the previous scenario, the combined use of measurements has better efficiency than other cases.

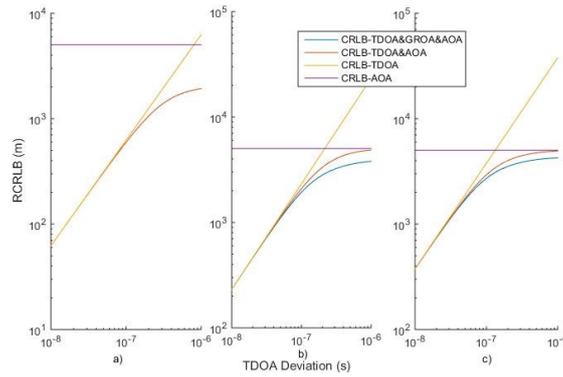


Figure 7: RCRLB vs TDOA standard deviation for a) decentralized processing of reference-surveillance channels, b) centralized processing of surveillance channels, and c) decentralized processing of surveillance channels.

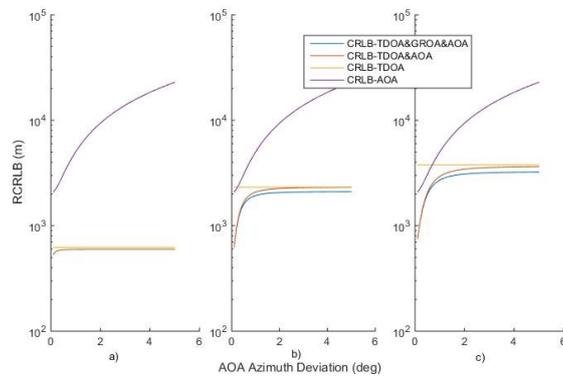


Figure 8: RCRLB vs AOA azimuth angle standard deviation for a) decentralized processing of surveillance-reference channels, b) centralized processing of surveillance channels, and c) decentralized processing of surveillance channels.

#### 4.2.3. Range dependency

To illustrate the dependence on range, we show the average effective range in the space. Figure 9 illustrates the mean of  $r_{T_a, Rx_j}^2$  for and receivers,  $r_{T_{x_i}, T_a}^2 r_{T_a, Rx_j}^2$  don't depend on receiver sensors arrangement. The receiver sensors are according to Table (2) in Figure 9 a) and are according to Table (3) in Figure 9 b). As illustrated, the Value is limited to  $8^9$ . The use of far distance arrangement of receiver sensors decreases effective range parameters. Thus, the SNR and accuracy of measurements improve.

## 5. Conclusion

This paper presents a variety of signal processing scenarios for target localization in multi-transmitter multi-receiver passive radar. The presented scenarios are investigated for the reception modes of the reflection signal with or without direct signal of the transmitter for the MFN and SFN transmitter networks. A variety of measurements are presented including TDOA, GROA, and DOA. Signal processing to calculate these measurements can be done by a decentralized processing in the receiver sensors or centralized processing in the central sensor. As mentioned, GROA and DOA measurements are obtained by decentralized processing of the surveillance signals in the receiver sensors. The TDOA measurements can be calculated under three different scenarios. These scenarios include decentralized processing of reference-surveillance signals at the receiving sensors, centralized processing of the surveillance signals at the central sensor, and decentralized processing of

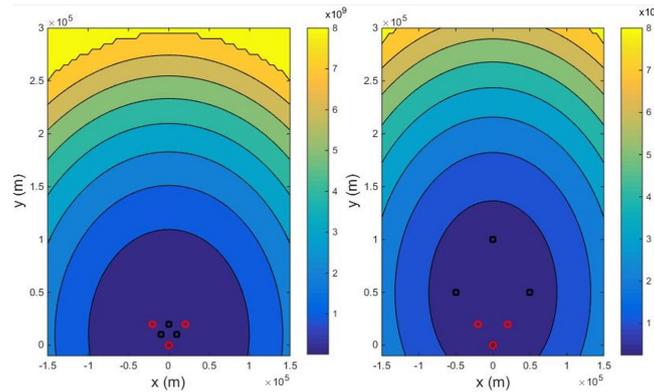


Figure 9: Mean of Effective Range on plane  $x$  and  $y$  for a) receiver sensors of Table (2) and b) receiver sensors of Table (3).

the surveillance signals at the receiving sensors. The decentralized processing scenario of reference-surveillance signals requires the simultaneous reception of the direct signal of the transmitter and the target reflections. In centralized processing of surveillance signals, sampled signals at the receiver sensors must be dispatched to the central sensor. In the decentralized processing scenario, the receiver sensors' surveillance signals must be sampled synchronously in terms of time. The low band of estimation error is presented as a criterion for evaluating these passive radar localization scenarios. The proposed CRLB is provided for all scenarios and types of measurements used for target localization including TDOA and/or GROA and/or AOA. As shown in the simulation results, different combinations of measurements always lead to better accuracy than single use of them. Also, given the different scenarios of receiver sensor arrangement, centralized and decentralized processing of surveillance signals with receiver sensors arrangement at a far distance outperform close arrangement scenarios. The proposed method can also be used to select the optimal arrangement for a given area and the known network of transmitters.

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